Contract Report: CR-2003/11

March 2003

Report: CR-2003/11

A protocol for the establishment and operation of LTPP sections - 1st Draft

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DOCUMENT RETRIE	VAL PAGE		Report No: CR-2003/11
Title: A protocol fo	r the establishment and ope	ration of LTPP section	ons - 1 st Draft
Authors: D Jones an	d P Paige-Green	,	
Client:	Client Reference No:	Date:	Distribution:
Gautrans	CR-2003/11	March 2003	Client Confidential
Project No: TIK03	OE2: Infrastructure Eng	ineering	ISBN:

Abstract:

This document describes a protocol for establishment and operation of long-term pavement performance (LTPP) sections, including those linked to HVS tests. This is detailed under the following headings:

- Linking LTPP to HVS data collection
- Management and responsibilities
- Site location and establishment
- Data collection
- Reporting criteria

A set of data capture forms is provided.

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Long term pavement performance, LTPP, APT, HVS

Proposals for implementation:

None

Related documents:

None

Signatures:

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Language Editor

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TERMS OF REFERENCE

CSIR Transportek was requested by Gautrans to develop a protocol for the establishment and operation of LTPP sections. The terms of reference for the study were to:

- Undertake a literature review on other LTPP studies
- Develop an appropriate protocol linking to the protocol already developed for HVS testing
- Develop appropriate data specifications for monitoring
- Prepare a report detailing the study and the recommended protocol.

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1. INTRODUCTION

Long-term pavement performance (LTPP) programmes are established to support a broad range of pavement performance analyses leading to improved engineering tools to design, construct and manage pavements. Most current LTPP programmes focus on the calibration of pavement performance models used in pavement management systems. It is also recognized that the link between accelerated pavement testing (APT) and inservice pavement performance is through LTPP studies. While APT can, and does, provide significant data for analysing and predicting the effects of traffic loading on the performance of various materials, it is not always capable of capturing environmental and other long-term effects. It is only when comparisons of LTPP and APT are available that there will be greater confidence in the interpretation and use of APT results for long-term performance prediction.

Hence the need has long been recognised for establishing LTPP test sections linked to existing and future APT sections, so that the long-term performance of the test pavements can be linked to their performance under APT. However, in South Africa, sustained long-term funding for this type of program has not been forthcoming and the programs have thus never been fully initiated, with LTPP studies mostly being undertaken on an ad hoc basis only. LTPP sections have, however, been identified for calibrating pavement deterioration models for pavement management systems in Gauteng and the Western Cape and are being monitored at routine intervals.

There is renewed interest in linking APT to LTPP worldwide, given the increase in the number of APT facilities and the need for accelerating the implementation of new technologies that will reduce the cost of infrastructure provision and rehabilitation, withstand increasing numbers of axles, axle weights and tyre pressures and minimise traffic disruptions.

In order to ensure that models and pavement design specifications determined from the data collected during APT and/or LTPP programmes are reliable, it is imperative that the data is collected in a systematic, consistent and correlatable manner. Protocols are therefore necessary to ensure that this is achieved.

While a protocol has already been developed for the establishment and operation of HVS test sections for Gautrans, it is now necessary to develop an LTPP protocol that provides a consistent approach to data collection, whether associated with HVS sections or stand alone sections.

This documents provides a protocol for the establishment and assessment of LTPP sections and has been developed to provide consistency with data collected from HVS testing.

1.1. Background

As part of this project an inception report¹ was written to evaluate current local and international practice as an input to better understanding the specific needs for a South African LTPP protocol. The project inception report is given in Appendix A and highlighted the following.

- Some LTPP work has been initiated in South Africa. Despite a draft general LTPP protocol (not specifically related to HVS tests) being proposed, this has not been implemented.
- The most prominent LTPP work in South Africa has been that related to the calibration of the HDM models for pavement management systems.
- A number of revisions of procedures for assessing the calibration sections for pavement management systems have been undertaken.
- Various ad hoc project-specific LTPP experiments have been carried out.
- A detailed protocol for LTPP work was devised in the USA for the SHRP program.
- The protocol used in the Australian APT/LTPP programme is based on the SHRP system.
- No other protocols were located.

Based on the review, it was concluded that a detailed framework taking into account specific local (southern African) problem areas was required, with an emphasis on providing data that is consistent with that collected during past and future HVS tests.

1.2. Scope

The idea of using LTPP sections to establish a link to real world conditions is not new, and thus this study builds on existing protocols, and, in particular, the FHWA SHRP LTPP and Austroads LTPP/ALF testing programs, which are the most comprehensive LTPP studies that have been undertaken. However, because the South African LTPP sections need to be assessed in terms of pavement performance for pavement management systems, comparison with HVS predictions and general performance for specific

assessments, the protocol will be formulated to use South African test methods and, where applicable, providing consistent data related to HVS-type testing procedures.

This protocol is presented under the following sections

- Linking LTPP to HVS data collection
- Management and responsibilities
- Site location and establishment
- Data collection
- Reporting criteria

2. LINKING LTPP TO HVS DATA COLLECTION

2.1. Introduction

HVS testing is an important and useful tool providing short-term pavement behaviour data. The results of LTPP testing differ in format and probably content. Although these are the ultimate data for inferring pavement performance and as many LTPP sections as possible should be developed, the cost of maintaining and monitoring them is high and significant additional data is available for HVS work.

Any protocol developed for LTPP testing must thus be compatible between the two techniques in order to make use of the available data accumulated from HVS testing.

Although the HVS is a very useful piece of equipment, and gives strong indications of pavement performance, a number of inherent deficiencies affect the outputs. These include:

- HVS testing covers a 1.0 m wide test section with a normally distributed loading pattern. In practice, traffic is not confined to the same one metre and although the distribution is still probably normal, it is expected that the distribution curve is flatter and wider.
- The HVS tests an 8.0 m long section with a uniform load in both directions. In practice, a road would be trafficked in one direction with variable loads. It should be noted, however, that the HVS can test unidirectionally, but the testing time is approximately doubled.
- The HVS operates at a repetitive high load, unlike the varying loads typical on roads
- The relaxation period on the test section is almost constant in the middle of the section, but varies from minimum to maximum near the two ends.
- During the hottest period of the day (probably the most damaging to the road) the test section is predominantly in the shade of the machine.
- The HVS wheel tests the road at a constant speed, unlike a normally trafficked road where vehicles travel at differing speeds.
- The HVS testing period is relatively short and does not take into account fluctuating moisture contents in the pavement structure resulting from seasonal variation. At the end of the test, the moisture content of the sections is usually artificially raised to what is probably outside normally expected conditions, to induce failure.

- HVS testing primarily tests the behaviour of a pavement structure under a controlled loading regime, whereas LTPP programs assess pavement performance under actual conditions.
- The HVS wheel is not a driven wheel and therefore has potentially different tyrepavement interaction effects compared to the torque effects of the driven vehicles of heavily laden trucks.
- Although the HVS MkIV has a dynamic capability that provides more testing options, the expected profile and dynamic effects of new roads cannot be predicted during HVS testing and hence a realistic dynamic profile cannot always be simulated by the HVS.

There is no doubt that an understanding of pavement behaviour is the basis for understanding pavement performance. The performance affects the costs of maintaining the road and operating traffic on it. LTPP is the only practical means of linking these two aspects. It is therefore essential that the protocols for HVS testing and LTPP testing ultimately provide comparable information. For direct comparison, monitoring of the same characteristics using the same equipment as far as practically possible should be carried out. The possible use of the data for other applications, such as calibration of HDM models, should be taken into account when planning HVS-LTPP monitoring programs.

The layout and requirements of individual LTPP sections may differ significantly, depending on the specific objective of the assessment. Monitoring should, however, be in line with this protocol as far as possible with additional requirements being satisfied as necessary.

2.2. Data Collection

There is general consensus on the performance characteristics of roads that should be assessed in order to understand the road pavement behaviour in the short-term and performance in the long-term.

Routine field-testing and monitoring of these characteristics, however, has resulted in the development of numerous techniques over the years, these being improved on an ongoing basis. The results obtained from measurements of a single property, but using different equipment or methods, are not always directly comparable (eg RSD, FWD and Deflectograph deflection measurements). For this reason, it is essential that as a minimum, only directly comparable or well-correlated assessment techniques are used for LTPP experiments.

Specific equipment has evolved to fulfil the measurement need of various behavioural properties during HVS testing. This has often involved expensive research and development resulting in sophisticated equipment fulfilling all the desired needs. The same parameters should thus be assessed in the same way on LTPP sections in order to ensure the required linkage. Additional techniques can be used for specific requirements on LTPP sections to complement the minimum requirements. However, these need to be calibrated against the prescribed techniques. It should be noted that, because of the limited area monitored during HVS testing, certain of these techniques may not be practical over the full area of an LTPP section (eg longitudinal profile).

A precise record of the wheel loading is recorded on every HVS test. In order to accurately relate performance of LTPP tests to that of HVS sections, it is imperative that accurate loading data is also available for the LTPP sections. The installation of permanent traffic recording equipment on each LTPP section is therefore strongly recommended.

The minimum data measurement requirements prescribed for LTPP sections have been partly based on the requirements for HVS tests and are listed in Table 2.1.

With ongoing development in measurement and analysis techniques, it is likely that some of the recommended methods could be improved or replaced during the life of the LTPP sections. It is imperative that any new technique adopted is carefully calibrated against the existing technique on all sections before it is replaced.

2.3. Laboratory and Field Testing Requirements

Where LTPP sections are established in association with HVS tests, the laboratory testing program currently followed for HVS tests should be expanded to include the LTPP test program. These tests will form the basis for comparison with later field tests. The actual tests carried out will depend on the type of pavement and surfacing being tested and the reason for carrying out the test. A testing program should be specified in the project brief.

LTPP sections that are established for other purposes should have testing programs specified in the project brief with the minimum testing requirements shown in Section 5.4.

Table 2.1: Minimum measurement requirements for LTPP sections

Property Visual assessment Transverse profile	LTPP Modified TMH9/HDM Calibration guide Straight edge & wedge/electronic straight edge	HVS Description of cracks Laser profilometer	Justification for difference TMH-9 is the standard visual assessment procedure. Additional information on cracks is captured to allow use of sections for HDM calibration. Full lane width is too wide for laser profilometer. Stabilization of measurement datums would also be difficult
Longitudinal profile Deflection	Calibrated profilometer RSD, FWD	Straightedge RSD	LTPP section is too long to measure with straightedge. IRI measurements can be used for calibration of HDM models FWD used routinely in network analysis in Gauteng
Permanent deformation Density	MDD Dual-probe strata gauge	MDD Dual-probe strata gauge	
Moisture content	Dual-probe strata gauge/gravimetric	Dual-probe strata gauge	Gravimetric moisture contents will be used to calibrate moisture content on the strata gauge
Pavement temperature	Temperature buttons	Temperature buttons	
	Weigh-in-motion	HVS	
vveamer details	Weather station	Weather station	

3. MANAGEMENT AND RESPONSIBILITIES

3.1. Introduction

LTPP studies, as the name implies, are long-term and should essentially run for the design life of the road and even through rehabilitation. Therefore in many cases individuals who initiate a study are unlikely to be involved at the end of the service life of the road. For this reason, roles and responsibilities need to be clearly defined and suitable posts identified within the Authority or Agency responsible for the LTPP sections with appropriate additions to job descriptions and key-result areas.

3.2. Staffing

The following minimum staffing requirements are recommended (Figure 3.1). Given that there will, in all likelihood, only be a relatively small number of LTPP sections, responsibilities will probably be incorporated into existing posts.

- Project director
- Project manager
- · Field technician
- Technician's assistants
- Database manager

The project director and project manager are Road Authority/Agency posts. If other posts are contracted out, then the contractor should also be required to appoint a project manager to assume responsibility and accountability for their staff and to liaise directly with the Road Authority/Agency project manager.

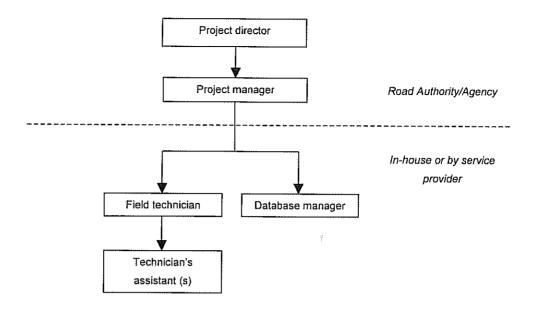


Figure 3.1: LTPP staff organisation chart

3.2.1 Project Director

The Project Director should have the following responsibilities for which he/she should be held accountable:

- Develop a strategic LTPP programme and experimental design
- Authorise the establishment of LTPP sections
- Motivate, justify and ensure sustainable funding
- Overall programme management and accountability
- Quality management of outputs
- Strategic management and implementation of findings
- · Industry liaison, coordination and feedback

3.2.2 Project Manager

The Project Manager should report to the Project Director and should have the following responsibilities for which he/she should be held accountable:

- Liaison with Project Director and HVS Project Manager for HVS-LTPP sections
- Site demarcation and establishment
- Site management and environmental, health and safety management for LTPP operation
- Calibration and accreditation of instrumentation, procedures and facilities
- Management of laboratory testing and control sample storage
- Appointment and management of other resources (eg FWD and traffic information)

- Training and calibration of the Field Technician
- Liaison with the Database Manager to ensure that data is useable and in the correct format
- · Analysis of results and reporting
- Management of maintenance interventions

3.2.3 Field Technician

The Field Technician should report to the Project Manager and should have the following responsibilities for which he/she should be held accountable:

- · Safety of field assistants and road users on site, including traffic control
- · Site markings
- Instrumentation
- Routine monitoring and timeous presentation of required results to the Database Manager
- Sampling and laboratory testing
- Ordering of commercial services (eg FWD)
- Reinstatement of sample holes and checking previous reinstatements
- Feedback on changes in appearance and performance

3.2.4 Technician's Assistants

The Technician's Assistants report to the Field Technician and assist in traffic control, site measurements and data capture duties as required.

3.2.5 Database Manager

The Database Manager should report to the Project Manager and should have the following responsibilities for which he/she should be held accountable:

- Timeous and accurate capture of data
- Database maintenance
- Facilitate report printing and distribution in suitable formats
- Ensure long-term availability and accessibility of all records in the database

Given the long-term nature of LTPP programmes, it is recommended that the database is kept in-house (ie at Gautrans) to prevent problems (eg lost data because of computer and software compatibility) associated with switching between contractors.

3.3. Other Resources

Other resources required for the monitoring of LTPP sections that fall under the responsibility of the Project Manager include:

- · An accredited laboratory
- Calibrated instrumentation and monitoring equipment as specified

3.4. Database Management

With projects of this nature and the rapid developments in the Information Technology arena, conscientious and regular attention to the entire database will be necessary to ensure that it is always accessible using current hardware and software. Considerable useful information on various road projects collected in the past has been lost or become unusable due to poor or erratic database management. The database must be comprehensively backed up regularly and these backups must always be upgraded when new hardware and software is installed.

The LTPP and HVS databases should be separate but compatible in order that the results from both systems can be directly compared or analysed together.

In order to facilitate the use of the information in the databases by authorised individuals, Internet access should be considered as part of the database development.

3.5. Funding

Unless sustainable funding can be guaranteed for an LTPP program, early investment in the setting out and monitoring of sections can be of little ultimate benefit. Many potentially useful experiments that would have gained significantly by long-term monitoring have not produced the desired results because of erratic or no sustainable funding.

In this protocol, the onus for ensuring sustainable funding is placed on the Project Director. This person will require significant support in the form of a long-term contractual agreement that should not be prejudiced by inevitable staff changes.

In order to reach these agreements, it will be necessary to estimate the annual cost of sustaining the program. Table 3.1 lists the typical components of the establishment,

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Table 3.1: Typical components of an LTPP monitoring program

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Equipment			MDD	Temp buttons	Aluminium tube	Sign boards	Paint	DCP points	FWD	Profilometer	Lab testing	Truck	Cold mìx		Truck	DCP points	FWD	Profilometer	Cold mix		
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Units	(Days)										***										
Manpower			Project director	Project manager	HVS engineer	Field technician	Field assistants	Travel	S&T						Project manager	Field technician	Field assistants	Travel	S&T		
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4. SITE LOCATION AND ESTABLISHMENT

4.1. Section Location

4.1.1 Existing Sections

Thirty-seven HDM calibration sections have been identified for use by Gautrans and are currently being monitored on an annual basis. Specific criteria relevant to the selection of HDM calibration sections were followed to identify the sections.

Provision has been made for LTPP sections adjacent to HVS sections at a number of sites. Although no routine monitoring is being carried out on these sections, they could be incorporated into an LTPP program if required.

4.1.2 New Sections

The identification and selection of LTPP sections will depend on the specific criteria and requirements of that investigation. The following general issues should, however, be considered when selecting sections:

- Sections should be representative of the issue being investigated and results
 obtained from these sections should be representative of other roads with similar
 conditions.
- The establishment of the section should not pose a safety hazard to road users, or be so positioned that the safety of the persons monitoring the section is jeopardised.
- The road on which the section is being located should not be maintained, rehabilitated or resealed within the planned monitoring period, unless assessment of that intervention is part of the monitoring programme and prior warning is given to the LTPP Project Manager.
- Sections should be located as close as possible to traffic counting/weigh-inmotion stations, unless a station is incorporated into the section.

4.1.3 HVS-LTPP Sections

The LTPP section should be adjacent to or within 100m of either side of the HVS test section provided that the features (pavement structure and topography) are exactly the same and that the same criteria used to select the HVS section (uniformity, representivity and safety) are used to select the LTPP section (Figure 4.1). When selecting the HVS test section, factors that may have an impact on the successful monitoring of an adjacent LTPP section must be considered. For example the change from cut to fill would not have an impact on the short HVS section, but could have a significant impact on an LTPP section. Areas to avoid include cuts, high fill, sharp bends, large culverts, etc.

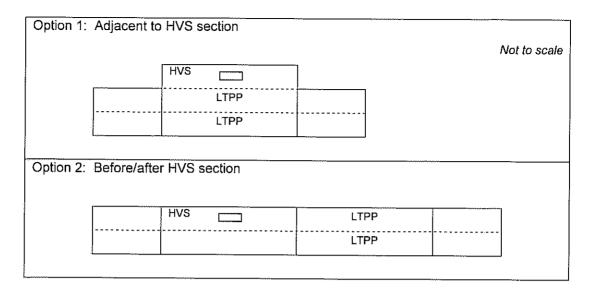


Figure 4.1: Options for location of LTPP sections

HVS Test Section Selection

HVS test sections are selected on the basis of pavement deflection measurements, as-built data and the structural characteristics of the specific test sections. Section identification is the responsibility of the project engineer, assisted by the HVS technician and in consultation with the project manager. The project manager and project engineer choose the frequency of deflection measurements, typically between one and three metre intervals as set out in the deflection measurement test programme. The Road Surface Deflectometer (RSD) is primarily used for deflection measurements, although Falling Weight Deflectometer (FWD) measurements may also be used.

Dynamic Cone Penetrometer (DCP) tests may also be used in the section selection to identify uniform areas and to give an indication of the pavement layer thickness. These measurements are used to validate as-built data or core measurements for positioning insitu pavement monitoring instruments.

4.2. Section Numbering

Each LTPP section should be assigned a unique number for management purposes. No formalised numbering system is in place for LTPP sections in South Africa. The HDM calibration sections are currently identified simply by a Section number of 1 through 39. Although this is probably sufficient for staff directly involved in that study, additional information in the number would facilitate management and data retrieval. A centralised list should therefore be initiated, using the following format:

Type of LTPP section:

R (Routine), H (HVS), C (Calibration)

Section number:

Consecutive numbers in order of section adoption

Year:

Year of construction or commencement of monitoring

Province:

Province in which the section is located

Road number

Example:

R1/03-G-P158/2 (The first routine section, constructed in

2003 in Gauteng on Road number P158/2)

C1/93-L-P1/3 (Calibration section No1, identified in 1993,

located in Limpopo on Road P1/3)

The chainage and direction of survey (positive or negative) should be linked to the section number in the database.

4.3. Section Layout and Marking

4.3.1 Existing Sections

The HDM calibration sections, on two-lane roads, are 500 m long and cover the entire road width including shoulders. On dual carriageways, the slow lanes, including shoulders, are monitored in both directions. Each section is subdivided into ten 50 m subsections. No destructive tests are carried out. The calibration sections are identified by signboard with section number and direction of survey. Subsections are located with a measuring wheel or tape. A typical layout is illustrated in Figure 4.2.

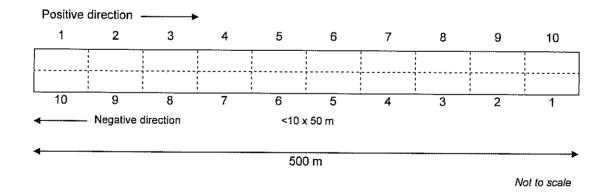


Figure 4.2: Layout of HDM calibration sections (two lane road)

No formalised section layout has been followed for other ad hoc LTPP sections or for the LTPP sections built adjacent to HVS test sections.

4.3.2 New Sections

The HDM calibration sections are 500 m long to allow a representative riding quality evaluation. However, monitoring long sections is a time consuming and therefore expensive undertaking. Therefore, a 200 m section is proposed for LTPP assessments, however, an additional 150 m can be demarcated on either side of the section for fuller riding quality assessments. Each 200 m section should be full-lane width and should consist of the following panels (Figure 4.3):

- 2 No 20 m panels (A and C) at either end for destructive testing (DCP, density and moisture content
- 1 No 10 m panel (B) in the middle for destructive testing (DCP, density and moisture content
- 10 No 15 m panels (1 -5 and 6 10) for general performance assessment

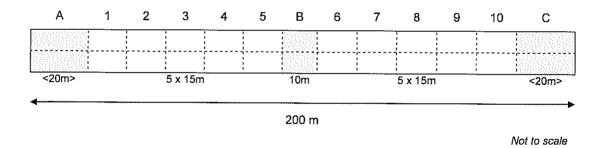


Figure 4.3: Layout of LTPP section (one lane width)

The GPS coordinates of the start of Panel A, centre of Panel B and end of Panel C of each LTPP section and the chainage at the beginning and end of each section should be taken and recorded in the database to facilitate location.

Each LTPP section should be marked as follows:

- Signboards with the LTPP section number should be erected at either end of each section against the fence line. If two additional 150 m sections are incorporated for riding quality measurements, additional signs should be erected at the start and end point as well.
- Each section should be demarcated and numbered with white road marking paint
 as shown in Figure 4.4. Locator points for the RSD and FWD deflection
 measurements should also be painted. These are situated in Panels 1 to 10 in
 each wheel track and in Panels 2, 4, 7 and 9 midway between the wheel tracks
 as follows:
 - RSD 5.0 m from the beginning of each Panel

 FWD - 5.0 m from the end of each Panel (an RSD should be done at this site before the FWD test to check for consistency between the two sites and to calibrate the two testing techniques for that section)

A "map" of each section should be drawn after completion of the demarcation and filed at a central point to facilitate future assessments.

4.4. Instrument Installation

No LTPP sections, including the HDM calibration sections, are currently instrumented. Instrumentation on new LTPP sections will be experiment dependent, but should be considered in order to obtain useful data about the performance of the pavement.

Instrumentation on the LTPP section should be installed to the same standard as that specified for HVS test sections, by experienced and competent technicians. On HVS-LTPP sections, instrumentation should be installed at the same time as that on the HVS section.

Instrumentation will include Multi-depth Deflectometers (MDDs) and temperature buttons. In addition to the instrumentation, holes, lined with a thin aluminium tube, should be drilled and capped in Panels A, B and C for density measurements. A permanent weigh-in-motion apparatus should be installed after the section. Additional instrumentation can be installed at the discretion of the Project Director.

Instruments should be installed as follows (refer to Figure 4.5). Note that the outer wheel path is selected visually by the Project Manager, or taken as being 1.0 m from the road edge or shoulder marking if the position of the wheel-path is not clear.

- 3 No Multi-depth Deflectometers in the outer wheel path as follows:
 - Panel A 1.0 m from boundary with Panel 1
 - Panel B 1.0 m from boundary with Panel 5
 - Panel C 1.0 m from boundary with Panel 10
- 9 No permanent holes for dual-probe hydrodensity meter in the outer and inner wheel tracks and on the centreline as follows:
 - Panel A 5.0 m from boundary with Panel 1
 - Panel B 5.0 m from boundary with Panel 5
 - Panel C 5.0 m from boundary with Panel 10
- 3 No temperature buttons midway between the wheel paths and adjacent to the hydrodensity meter holes

 1 No Weigh-in-motion system within the first 100 m after the LTPP section, unless a permanent station already exists between the site and the next/previous intersection/off-ramp.

Instructions for calibration and installation of these instruments are provided in Appendix B.

4.5. Weather Station

A weather station comprising at least a thermometer (maximum and minimum) and a rain gauge should be erected as close as possible to the section. If the site is in a rural area, the most appropriate would be the closest farm. Measurements and reporting would have to be negotiated with the landowner. If the site is within a municipal boundary, then the closest official recording station can be used if no other suitable location can be found.

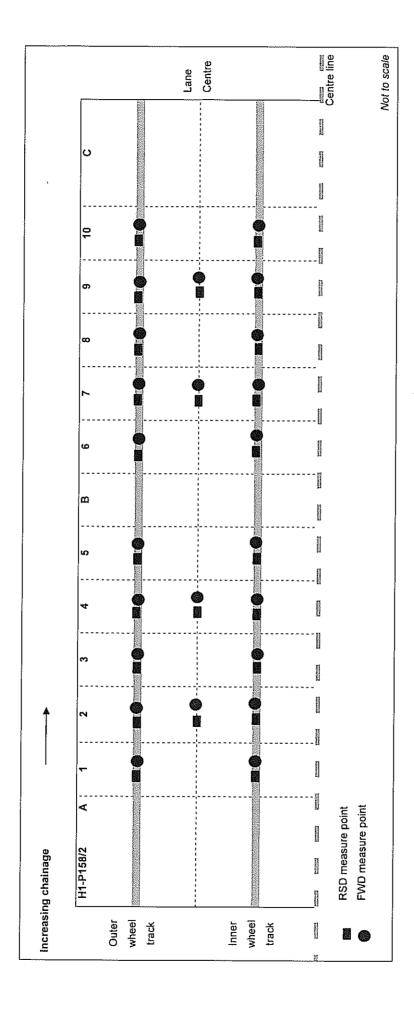


Figure 4.4: Section and measure point demarcation for LTPP sections

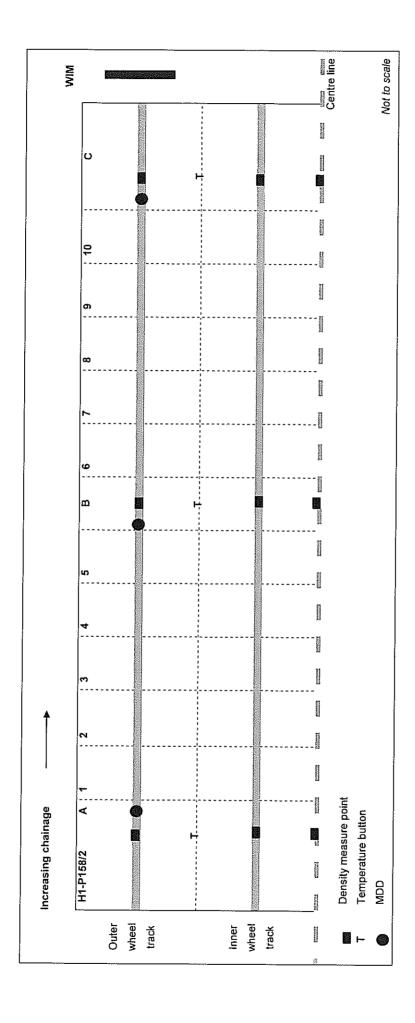


Figure 4.5: Instrumentation location for LTPP sections

5. DATA COLLECTION

5.1. Monitoring Standards

5.1.1 Visual Assessment

Visual assessments should be carried out on each panel according to TMH-9² and where appropriate, the Gautrans Visual Assessment Manual for the calibration of HDM-III/IV³, which is used in conjunction with TMH-9. Results should be recorded on an LTPP Visual Assessment Form (Form 1 in Appendix C). In order to link the LTPP performance to HVS tests, it is important to identify when the first cracks appeared, the nature of the cracking and how the crack pattern changed over time. Crack patterns should be linked to a cause wherever possible (eg change in deflection). Additional measurements as specified can also be taken to suit the needs of the experiment.

The Project Manger should calibrate the field technician assessors before each monitoring cycle (see TMH-9).

The following digital photographs should also be taken during each visit:

- A general view of the road from both ends (photographer stands on the outer limit of Panels A and C in the middle of the lane)
- Two photographs of each panel taken from the start and end of each panel in the middle of the lane. The two metre straight edge should be laid across the road midway between the FWD and RSD wheel track monitoring points as a scale.
- Photographs of any specific distress details should also be taken using the 2.0 m straight edge, or part thereof as a scale. Notes on the photographs should be made in the Notes section on the Visual Assessment Form.

Output

Completed visual assessment form.

5.1.2 Transverse Profile

Transverse profile should be measured with a 2.0 m straightedge and 1.0 cm wedge. If available, the electronic straightedge³ developed for the HDM calibration sections can also be used. The end of the straight edge should be placed in the marked centre of the lane, first in the direction of the road edge and then in the direction of the centreline, on each panel boundary. The following measurements should be taken:

 A profile of measurements every 100 mm from lane centre to road edge/centreline

- Maximum rut depth
- Rut width (measured with a tape measure).

Measurements should be recorded on the LTPP Profile Form (Form 2 in Appendix C).

Output

Completed transverse profile form.

5.1.3 Longitudinal Profile

Longitudinal profile should be measured with any instrument that provides an International Roughness Index (IRI) calibrated to specification for IRI. In South Africa, profile measuring equipment is calibrated on calibration sections, measured with rod-and level and against a Dipstick® profileometer. This instrument is also specified for longitudinal profile measurements in the United States SHRP LTPP program.

The average IRI of three runs, two in the increasing direction and one in the decreasing direction should be recorded. The profile of both wheel paths should be measured.

Output

Average IRI for each wheel path in each panel. If the data is recorded electronically, it should be provided in spreadsheet compatible format.

5.1.4 Density and Moisture Content

Density and moisture content should be measured with a dual-probe hydro-density meter in permanent holes drilled and lined with a thin aluminium tube (1.0 m) for this purpose in Panels A, B and C (see Figure 4.5). The holes must be sealed with an appropriate bung immediately after testing. Moisture contents measured with the hydro-density meter should be calibrated against a gravimetric moisture content sampled with a hand or power augur near the hole. Material representative of each layer should be sampled to the same depth as measurements taken with the hydro-density meter and the gravimetric moisture content compared with the recorded readings for at least the first six monitoring visits (ie three years) or until a satisfactory correlation has been obtained. The machine wet and dry densities and moisture content should be recorded for every 50 mm depth. These readings, together with the gravimetric moisture content and recalculated dry density should be recorded on the LTPP Density and Moisture Form (Form 3, Appendix C).

In order to ensure that there is no long-term influence on the moisture regime or density around the HDM holes, care must be taken in selecting the sampling sites (recommended at least 1.0 m from the hydro-density meter hole in a circular pattern). The holes must be

reinstated with shoulder gravel and tamped with a suitable rod and then the upper 30 mm sealed with cold mix asphalt.

Detailed instructions on the measurement of density and moisture are provided in Appendix B.

Output

Completed form Density and Moisture Content Form. Note that this form is only considered complete when the gravimetric moisture content and recalculated dry density have been captured.

5.1.5 Dynamic Cone Penetrometer (DCP)

DCP measurements should be taken approximately 1.0 m from the density/moisture content sampling areas in Panels A, B and C. Measurements should be recorded at 5-blow intervals to a depth of 800 mm. Cemented layers should be drilled if no penetration with the DCP is obtained. DCP tests should be done within 1.0 m of the HDM holes and subsequent tests should be carried out at least 1.0 m from existing sealed holes. Disposable cones should be used to prevent excessive disturbance during extraction of the apparatus. The use of disposable cones also reduces the chance that damaged cones will be used. However, cones should always be checked prior to the test being carried out. All DCP holes should be sealed with cold-mix asphalt (at least a 30 mm plug).

Results should be recorded on the LTPP DCP Form (Form 4, Appendix C).

Output

Completed DCP form.

5.1.6 Environment

Environment assessment will entail:

- Capturing weather details (daily rainfall, maximum and minimum temperature)
 recorded near the section or from a local weather station (Data captured on LTPP
 Weather Detail Form (Form 5 Appendix C))
- A visual assessment of the drainage of water from the road and away from the road according to TMH-9² (captured on the Visual Assessment Form)
- Downloading pavement temperature from the temperature buttons (temperature intervals of 120 minutes). This entails removing the button, downloading the information into a computer and then replacing the button. Data should be transferred to a spreadsheet before being submitted.

If recycled materials or non-traditional chemical additives are used in the road, additional environmental testing of the impacts on ground and surface water, soil and adjacent vegetation will have to be assessed according to a protocol developed specifically for the material being assessed. No protocol for environmental monitoring of LTPP and APT sections is currently available.

Output

Completed Weather Detail Form, Visual Assessment Form and spreadsheet of pavement temperatures.

5.1.7 Deflection

Deflection should be measured with both RSD and FWD at each of the points described in Section 4.4. The procedure for calibrating, taking and recording RSD measurements is detailed in Appendix B. Data is captured electronically. The procedure for FWD measurements will be instrument specific, but must be available for scrutiny. Both instruments must be calibrated according to the specification provided with the instrument, on the same section of road (RSD followed by FWD), with details of the calibration and name of calibrator included on the result form.

The following load properties should be used:

Plate pressure/drop height: 550 kPa

Plate diameter: 150 mm

Sensor offset positions: 0, 200, 300, 600, 900, 1 200 and 1 500 mm

• Load impulse: half sine 25 - 30 millisecond

Output

Spreadsheet with the following data:

- Instrument
- Panel number
- Position
- Load data
- Pavement and air temperature
- Peak deflection
- Deflection at offsets

5.1.8 Permanent Deformation of Pavement Lavers

Permanent deformation should be determined from the multi-depth deflectometers (MDD) installed as prescribed (Section 4.4) in Panels A, B and C. Information should be downloaded and submitted in spreadsheet compatible format.

5.1.9 Traffic

Traffic data should be obtained from the nearest traffic counting station. Since traffic data is essential for the accurate modelling of pavement behaviour, the installation of permanent weigh-in-motion systems in the vicinity of the LTPP section, as prescribed in Section 4.4, is strongly recommended. The following minimum traffic data needs to be recorded:

- Number of vehicles
- Number of vehicles per weight classification (2 tonne intervals)
- Number of axles per vehicle
- · Mass of each axle for vehicles with axle mass greater than 2 tonnes
- Distribution of vehicles with axle mass greater than 2 tonnes
- Vehicle speed
- Vehicle length
- Cumulative equivalent standard axles (E80's)

Tyre pressures on heavy vehicles should be recorded at existing weigh bridges at regular intervals and captured in the database.

Output

Summary of data on a monthly basis in spreadsheet compatible format.

5.1.10 Test Pits

Test pits should only be excavated on LTPP sections to assess the cause and attributes of major failures that require rehabilitation, or if the road is scheduled for reconstruction or rehabilitation. The size and depth of the test-pit will depend on the attributes being assessed. Pits should be profiled immediately after excavation.

The test pit profiles should be fully described according to the Jennings, Brink and Williams standard⁴. However, additional information on the nature of the interlayer boundaries (deviations and conditions, eg ruts and cracks) should also be included. For cemented layers, it will be important to assess the in-situ condition of the stabilized layer. This is best done using a phenolphthalein spray. Observations should be recorded on an LTPP Test Pit Form (Form 6, Appendix C).

Samples should be removed from each layer in both wheel tracks and the centreline. Sufficient sample should be removed to satisfy the requirements of the tests that will be carried out. If failures are being investigated, material from the failed area in the layer should be sampled.

If test pits are excavated during the service life of the road for any reason, they should be carefully reinstated using material and layer thicknesses conforming as closely as possible to those in the road. Careful sealing of the surface, to prevent the ingress of water and inducement of axle hop, must be carried out.

Output

Completed LTPP Test Pit From

5.2. Sampling and Reinstatement

Samples should only be removed from Panels A, B and C. If a significant failure occurs in one of the other panels, a test pit can be excavated for investigation purposes. That panel should then be excluded from further evaluations, but the repair should be of such quality that it does not affect the performance of adjacent sections.

All sample holes and test pits must be properly reinstated. This will include:

- Replacing similar material to that excavated from each layer and compacting it to the specified thickness and density
- Effectively sealing the excavation ensuring that no water can penetrate into the base
- Levelling the surface of the patch such that the riding quality of the section is not affected and that dynamic bounce in vehicles that may affect the adjacent sections is not introduced
- Monitoring the patches on all subsequent visits to ensure that water is not penetrating the patch and that the patch is still level with the surrounding surface

5.3. Monitoring Program

Each section should be monitored at six monthly intervals, in May and October. More frequent assessments can be made if required, once distress/failure is initiated.

The HDM calibration sections are currently assessed on an annual basis at the end of the dry season (August/September in Gauteng). FWD measurements were taken at project initiation and after approximately five years. No plan for regular FWD measurements is in place.

5.4. Laboratory Testing

Laboratory testing is an integral component of APT and LTPP programs and is carried out to fully understand the characteristics of the pavement material. It is essential that the properties of the material at time of construction (or section initiation) are fully identified and recorded to allow comparison over time. As built records are unlikely to provide the level of data required. Laboratory testing should be carried out in an accredited laboratory.

Testing programs should be initiated at the following intervals:

- Pre-construction/rehabilitation
- Post construction/rehabilitation
- In service (approximately half way through design life of experiment or pavement)
- · Rehabilitation/end of service

Details on the tests for LTPP sections are listed in Tables 5.1 to 5.4. For experimental monitoring, specific additional properties may need to be assessed, depending on the application.

Testing, such as durability and C and Φ is generally only applicable to base and sometimes subbase and will not be necessary for other layers. The durability testing method would need to be adapted for the material being assessed (eg glycol soaking for basic crystalline rocks and Venter Slake Test for mudrocks).

It is important that as much testing as can be practically done is carried out during the pre-construction and construction period as it is usually not possible to obtain representative samples of the unprocessed material at a later date. For this reason, it is also suggested that a control sample is collected and carefully stored for possible later testing. Representative samples should be removed from each layer.

	Recommen	Recommended laboratory testing for LTPP monitoring	g for LTPP monitori	bu	Table 5.1: Pr	Table 5.1: Pre-construction
	Surfacing	,			Base/subbase	
	Asphalt	Concrete	with the same of t	Treated	NAME OF THE PROPERTY OF THE PR	Granular
HMA	Seal		Cement/lime	Bitumen	Other	
Grading	Grading	Grading	Atterberg limits	Atterberg limits	Atterberg limits	Atterberg limits
10%FACT or ACV	10%FACT or ACV	Water absorption	Grading	Grading	Grading	Grading
Flakinėss/ALD	Flakiness/ALD	Organic	OMC/MDD	OMC/MDD	OMC/MDD	OMC/MDD
Sand equivalent	Sand equivalent	ACV or 10% FACT	CBR or UCS	CBR or UCS	CBR	CBR
PSV	PSV	UCS	ITS	ITS	CEC	10% FACT
Durability	Durability	Particle density	ICS	Stiffness	Hd	Flakiness
Binder viscosity	Binder viscosity	Shape and texture	Wet/dry brush	C and Φ	Modulus (E) and v	ARD/BRD/WA
Softening point	Softening point	Soluble salts	Accelerated carbonation	(10)	Durability	pH and conductivity
Penetration	Penetration	Mineralogy	E-modulus	1111.		Durability*
Adhesion	Adhesion	Sulphate soundness		, and the second se		C and Φ
Fatigue	Fatigue	E-modulus	North Comments of the Comments	ST TO THE STATE OF		Modulus (E) and v
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Film thickness	- interest		And the second s			
Binder chemistry			·		- Juny	, series de la companie de la compan
Stability			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, in the second		
*Appropriate for the n	*Appropriate for the material being used and the layer for which it is being used	for which it is being used	Trans.	TANK T	- Volumenta	

nmended labor	Recommended laboratory testing for LTPP	PP monitoring		Table 5.2: Post-construction	construction
		pp. min.	Base/subbase	ubbase	
E CO	Concrete		Treated		Granular
		rozzolanic	Bitumen	Other	
Cube strength		Atterberg limits	Grading	Atterberg limits	Atterberg limits
ITS	MO	OMC/MDD	OMC/MDD	Grading	Grading
Beam shrinkage		Field compaction	Field compaction	OMC/MDD	OMC/MDD
· ·	ĵ n c	UCS & ITS on cores	ARD/BDR	Field compaction	Field compaction
***************************************	Cen	Cement/lime content	UCS & ITS on cores	pH and conductivity	pH and conductivity
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1111			Binder content	- 1984;	n in the state of
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	Base/subbase	Treated	Bitumen	UCS & ITS on cores	Fatigue	Permeability					· VALLEY.			A Committee of the Comm					- Activity	
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Recommended labor	Surfacing	Asphalt	Seal	Binder viscosity	Softening point	Penetration	Ductility	Fatigue	Binder chemistry		and the second	1977	and the second s	AVANCE.		nggradu	2000	 2000		, invo
			HMA	Binder viscosity	Softening point	Penetration	Ductility	Fatigue	Permeability	Stability	Binder chemistry							de transcentina de la companya de la	- Province	

Table 5.4: Rehabilitation/end of service	, , , , , , , , , , , , , , , , , , ,	Granular				The state of the s				1,000 mg	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	, john tre	, , , , , , , , , , , , , , , , , , ,			To play the day of				production of the state of the
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6. REPORTING CRITERIA

All field monitoring and test data should be transferred to a set of clean forms, checked by the Field Technician and then the Project Manger before being presented to the Database Manager within 10 days of the assessment. Any accompanying laboratory test data should be completed and handed in together with the field data.

Other incidental laboratory testing associated with failures or rehabilitation/repairs will usually take longer, but should be collated and checked before being submitted to the Database Manager, as soon as possible after testing has been completed.

The database must be kept up to date with all available information. This information must be in the current software format and all data must be backed up in the same format. Past backups must all be updated along with any revisions of software or software version.

6.1. First Level Analysis

A first level analysis should be carried out after each monitoring, with plots between selected performance criteria (eg, peak deflection, IRI, rutting, rut depth) and environmental properties (eg traffic and rainfall).

6.2. Second Level Analysis

A second level analysis should be carried out every two years and should include:

- An evaluation of the structural behaviour
- The identification of any extraneous effects
- · The development and refinement of performance prediction models
- On HVS-LTPP sections, the relationship between LTPP and HVS performance for similar traffic loading periods

The ultimate objective of the analysis over time will be to develop models to predict the performance of the road as recorded in the LTPP monitoring. Accompanying HVS data can assist with this and/or can be extrapolated using the LTPP data to more accurately predict long-term performance.

7. REFERENCES

- 1. JONES, D. and Paige-Green, P. 2003. The development of a protocol for the establishment and operation of LTPP sections in conjunction with HVS tests: Inception Report. Pretoria: CSIR, Transportek. (Contract Report CR-2003/7).
- Pavement management systems: Standard visual assessment manual for flexible pavements. 1992. Committee of State Road Authorities. (Technical Methods for Highways, TMH9).
- 3. **Visual assessment manual for the calibration of HDM-III/IV**. 2001. Pretoria: Gauteng Department of Transport and Public Works. (Report RNMS/H/49/E, 2nd Edition).
- 4. JENNINGS, J.E., Brink, A.B.A. and Williams, A.A.B. 1973. Revised guide to soil profiling for civil engineering purposes in South Africa. **The Civil Engineer.** January 1973, pp 3-12.

APPENDIX A	
INCEPTION REPORT	

APPENDIX A: INCEPTION REPORT

copy of the inception report prepared for this study is included as a background reference.	

Draft Contract Report: CR-2003/7

February 2003

Draft Report: CR-2003/7

The development of a protocol for the establishment and operation of LTPP sections including those associated with HVS tests: Inception Report

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1. INTRODUCTION

Long-term pavement performance (LTPP) programmes are established to support a broad range of pavement performance analyses leading to improved engineering tools to design, construct and manage pavements. Most current programmes focus on the calibration of pavement performance models used in pavement management systems. It is recognized that the link between accelerated pavement testing (APT) and in-service pavement performance is through LTPP studies. While APT can, and does, provide significant data for analysing and predicting the effects of traffic loading on the performance of various materials, it is not always capable of capturing environmental and other long-term effects. It is only when comparisons of APT and LTPP are available that there will be greater confidence in the interpretation and use of APT results.

Hence the need has long been recognised for establishing LTPP test sections linked to existing and future HVS test sections, so that the long-term performance of the test pavements can be linked to their performance under HVS testing. However, in South Africa, sustained long-term funding for this type of program has not been forthcoming and the programs have thus never been fully initiated, with LTPP studies being undertaken on an ad hoc basis only. LTPP sections have, however, been identified for calibrating pavement deterioration models for local pavement management systems and are being monitored at routine intervals.

There is renewed interest in linking APT to LTPP worldwide, given the increase in the number of APT facilities and the need for accelerating the implementation of new technologies that will reduce the cost of infrastructure provision and rehabilitation, withstand increasing numbers of axles, axle weights and tyre pressures and minimise traffic disruptions.

In order to ensure that models and pavement design specifications determined from the data collected from LTPP and APT programmes are reliable, it is imperative that the data is collected in a systematic, consistent and correlatable manner. A protocol is therefore necessary to ensure that this is achieved.

In this report, LTPP protocols are reviewed and a framework for developing a local protocol for the establishment and operation of LTPP sites in general and in conjunction with HVS tests is discussed.

2. REVIEW OF LTPP PROTOCOLS

2.1. South Africa

Sources of information:

- Department of Transport reports by Bofinger and Shackelton
- Department of Transport reports by Paige-Green
- ISAP paper by Jooste
- Discussions with E Sadzik (Gauteng), M Henderson (Western Cape), R Lindsay (KwaZulu-Natal), D Rossman and M Yorke-Hart (Sanral), G van Zyl (Consultant), I Wolmarans (Consultant).

2.1.1 Previous Studies

Despite HVS tests being carried out in South Africa since 1976, an LTPP study was first initiated in South Africa in 1991, part of which entailed an investigation of the relationships between LTPP and HVS results¹. The terms of reference for the study were later amended to establish LTPP sites for data collection for pavement management systems. However, in the initial part of the study rut depth, cracking and peak deflection measurements recorded on HVS sections were compared with those measured a number of years later on adjacent LTPP sites. The following experiments were monitored:

- Road between Laudium and Erasmia (Pretoria)
- Road between Pretoria and Johannesburg International Airport (P157/1 and P157/2)
- Koeberg (TR77/1)
- Stellenbosch (MR8)

Another comparison was made between HVS results and actual performance on P157/1 by Jooste et al in 1996². Measurements included Dynamic Cone Penetrometer, (DCP), moisture and density, peak deflection and rutting.

Cracking

Bofinger made no reference to the method of assessing cracks, although it is assumed that TRH6³ was used (TMH9² was not published at the time of the study). During HVS tests, two types of cracking were noted, namely the existence of edge cracks and the appearance of cracks within the section. Under HVS loading conditions, the loaded wheel covers a section exactly 8.0 m by 1.0 m and the adjacent pavement carries no load of any type. On a normal road, there is no such distinct demarcation between parts of the

road surface that carry no wheel loads and a strip 1.0 m in width that carries all the applied loads. It is common, therefore, for edge cracks to occur in the HVS tests and, while these are noted, they have no comparable occurrence in normal road pavements¹.

At the time of writing the report¹ (1992), it was standard practice on HVS test sections to note the appearance of the first crack at each of the 16 equally spaced measuring points in each 8.0 m length. No other measurements such as the change in the width of the crack or the appearance of other cracks were noted subsequent to the first crack appearing. (The method of measuring cracks on HVS sections has since changed⁵ with daily monitoring and recording of crack development.)

On specific HVS sections, measurements of the horizontal and vertical movements were made across specific cracks with a Crack Activity Meter (CAM), but these have no corresponding measurements on sections of the road network. It was therefore concluded that the appearance of cracks or the relative movement across the faces of the cracks could not be used to compare the performance of pavements during HVS tests with their performance under the longer term conditions when a pavement is subjected to the loading of normal commercial traffic.

Jooste et al did not assess cracks as they considered it a difficult measure to compare in a quantitative manner because of the often-subjective nature of measurement and definition of cracks. This problem has largely been overcome with the use of digital photography.

Peak Deflection

In the earlier study, concerns were raised about data acquired from the adjacent pavements in that test results were not adequately documented or the location of the precise position of the deflection tests was not known (the substantial variations of the peak deflection within 1.0 m had been noted from the HVS tests and the exact locations of the points at which deflection values were measured were considered essential if peak deflections were to be used to denote the changes in condition of the pavement). Inspections of the deflection tests carried out during the selection of the exact site for an HVS test showed that none of the test points could be relocated precisely and repeat tests could not, therefore, be carried out at the same points. The variation in pavement response would introduce unacceptable errors in repeat deflection tests carried out in a similar area. Peak deflection values were therefore excluded from the study as a system for monitoring changes in the pavement structures with traffic.

In Jooste et al's study, Road Surface Deflectometer (RSD) and Falling Weight Deflectometer (FWD) measurements were taken and compared with the deflection measurements taken during HVS testing. No mention is made of the concerns raised

above. Furthermore, it was found that the HVS-predicted deflections compared well with the deflections measured after the road had been trafficked for 16 years.

Rutting

Bofinger believed that changes in the rut depth provided the best comparison of the condition of pavements loaded by the HVS and the road network adjacent to HVS test sections, where normal traffic loaded the pavement, although some problems were still encountered in quantifying the traffic loads that the pavement had carried in terms of standard axles. A relative damage coefficient of four was ultimately used. Substantial differences were noted between the rut ratios obtained in Gauteng (underestimated) and those in the Western Cape (overestimated). This was attributed to the different subbase types (cement in Gauteng, granular in the Cape).

Jooste et al found that the HVS rut curve compared well with the rut depth measured after actual traffic and 16 years of changes in environmental conditions. However, since the rut depths were in all cases very low, the strength of the conclusions that could be drawn was considered to be somewhat limited. However, it was concluded that environmental influences that were not included in the HVS testing did not cause significant changes in rut depth formation and that the rut depths that developed during HVS testing were very similar in magnitude and variation to those measured after a significant period of trafficking and seasonal changes in environmental conditions.

Other Studies

Paige-Green⁶ reported on the long-term pavement performance of 24 sections of low-volume road constructed with marginal base course materials. No standard protocols were followed with ongoing collection of specific data over a period of more than nine years in order to relate performance to pavement material properties and structure. A number of problems including the accurate assessment of traffic in terms of standard axles, significant fluctuations in moisture content (variance from predicted values), poor correlations between deflection and performance, and generally high variability in properties over short sections of road were noted.

A number of other LTPP studies have been carried out, mostly of an ad hoc nature to monitor various parameters. Most of these have been for pavement management purposes, rather that pavement design. In the past nine years, a number of sections in the Gauteng and Western Cape provinces have been identified and routinely monitored to calibrate pavement deterioration models (HDMIII) for pavement management systems. No attempt has been made to link HVS performance data and monitoring protocols (visual assessment, deflection (FWD) and riding quality (IRI)) and the database population is based on the data input requirements for HDMIII and HDMIV. A visual assessment guide was developed for monitoring the sections⁷. LTPP sections have been

purposely built adjacent to HVS sections since 1997 (Road 2388), although no official LTPP monitoring programme is being followed for these roads.

2.1.2 Site Establishment and Data Collection Protocols

Department of Transport - 1991

A draft protocol for LTPP section identification and monitoring was established as part of the 1991 South African LTPP study⁸ and included details on the following:

- Selection of test sections Guidelines, rather than a protocol, were provided on the criteria to be used for selecting sections and primarily focussed on the development of pavement deterioration models. These included level of traffic, age of the road, type of pavement, section layout and inventory data. Emphasis appeared to be on selecting sections that had not been tested with the HVS. The development of a detailed populated experimental design was not initiated as it was considered outside the scope of the study.
- Types and methods of test The following parameters were considered essential for the monitoring programme:
- Extent, degree and type of cracking
- Riding quality/road roughness
- Extent of patching
- Extent of bleeding/stone loss
- Rut depth
- Deflection characteristics
- Moduli/strengths (usually back-calculated from deflection data or from DCP)
- Surface characteristics (penetration, texture)
 In addition to the above routine assessments, detail on diagnostic testing for auditing purposes or in the event of ultimate failure of the pavement sections was provided. A number of material tests were proposed.

Details on the methods to assess the above parameters were provided. No visual assessment manual is prescribed. The recommended methods for assessing roughness (Linear Displacement Integrator, rod-and-level survey, rolling profilometer) are outdated. There was also some debate around deflection measurements, with an assumption that it would not be possible to get parties to agree on one testing method. It was therefore proposed that, as an absolute minimum requirement, deflection tests be carried out with the device that is normally used by the road authority in the region in which a particular road section is located and that every second survey be completed using both an FWD and a Benkelman Beam.

- Frequency of the monitoring operations Guidelines, instead of a protocol, were provided for frequency of testing, with intervals between tests largely left to the discretion of the road authority.
- Traffic loading data The following essential traffic parameters were identified:
- Axle load spectrum of the vehicles travelling on the section
- Axle configuration
- Speeds of the various categories of vehicle
- Range of tyre pressures used by each category
 Guidelines on the method and frequency of collection are given.
- Data storage and management Broad recommendations on general structure of the information management system, process of database population, database structure and software and access rights were made.
- Data analysis Data analysis is described as formal and informal. Formal
 analyses are those that must be carried out to achieve the ultimate goals of the
 LTPP programme. Informal analyses are typically those associated with
 research studies and usually investigate specific problems or phenomena. The
 following requisite formal analyses were identified:
- Variation with parameters over time
- Correlation between any two parameters (eg rut depth vs deflection)
- Correlation between wheel paths for any parameter
- Correlation between performance of different pavements or pavement types
- · Adequacy of data for the above tasks

Gautrans Visual Assessment Manual - 2001

In 1996, Gautrans commissioned a study on calibration of HDM-III models for local conditions. Thirty-six sections were identified and a Visual Assessment Manual written. The manual, which is used in conjunction with TMH-9², includes the following chapters as well as an example of the data collection form:

- Location and length of sections
- Section width
- Surface defects (cracks, ravelling, mechanical damage, shoving/slippage of the surfacing, binder condition and bleeding/flushing)
- Structural defects (cracks, pumping, patching and potholing)
- Functional evaluation (assessed using TMH-9)
- Rutting

No detail is given on the selection of new sections, traffic counts or the measurement of deflections (two deflection measurements (FWD) have been taken during the course of the study). Destructive testing (density, DCP, moisture measurements) is not discussed.

2.1.3 Protocol for HVS Instrumentation, Data Collection and Data Storage

The CSIR has managed Heavy Vehicle Simulator (HVS) operations in South Africa for the past 25 years. During this period, experience in the collection and storage of pavement performance data under accelerated pavement testing has been gained. Current norms relating to quality management of processes and products necessitated the consolidation of these processes into a protocol for use in future HVS projects. A protocol⁵ was therefore recently prepared and is currently under review. The protocol covers three key aspects of HVS operations, namely:

- Instrumentation used for pavement performance monitoring and protocols related to installation
- Data collection protocol
- Storage of collected pavement performance data

Site selection criteria, test section identification, calibration methods and operational instructions are also described in the document.

Any protocol document prepared for the comparison of HVS and LTPP sections in South Africa would need to take the HVS protocol into consideration to ensure that similar parameters are measured in a similar way.

2.2. United States

Sources of information:

Federal Highways Administration Website and reports

2.2.1 Background to SHRP LTPP Program

The United States Strategic Highway Research Program (SHRP) was a five-year, US\$150M undertaking. It was the largest single highway research program ever conducted in the United States and represented the most concentrated investigation of highway problems undertaken anywhere in the world. SHRP research addressed four technical areas of investigation:

- Asphalt
- Concrete and Structures

- Highway Operations
- Long-Term Pavement Performance (LTPP)

The LTPP component of the program embraced the total range of pavement information needs. It drew on knowledge of pavements currently available and sought to develop models that would better explain how pavements perform. It also sought to gain knowledge of the specific effects on pavement performance of various design features, traffic and environment, use of various materials, construction quality and maintenance practices.

Despite SHRP's five-year program being formally completed in 1993, the nature of LTPP is such that this aspect of the program will have a duration of about 20 years. To facilitate this, the management of the LTPP study was taken over by the US Federal Highway Administration (FHWA).

More than 2 400 sections representing a diverse range of physical, environmental and traffic conditions are being investigated in the program. The scope of the program allowed other countries, including Canada and Australia, to participate in the program.

The United States LTPP program has the following specific objectives9:

- Evaluate existing design methods
- Develop improved design methodologies and strategies for the rehabilitation of existing pavements
- Develop improved design equations for new and reconstructed pavements
- Determine the effects of loading, environment, material properties and variability, construction quality and maintenance levels on pavement distress and performance
- Determine the effects of specific design features on pavement performance
- Establish a national long-term pavement database to support SHRP objectives and future needs

Monitoring of the more than 2 400 sections started in 1989. The program was initially set up with three subsections, namely:

 General pavement studies (GPS) monitoring a 160 m section selected from a full factorial experimental design incorporating the following primary and secondary factors:

Primary	Secondary
Subgrade (fine/coarse)	Asphalt concrete (AC) thickness
Traffic (medium/heavy)	AC stiffness
Temperature (freeze/non-freeze)	Structural number of base and subgrade
Moisture (wet/dry)	Portland cement concrete (PCC) thickness
	Joint spacing

 Specific pavement studies (SPS) monitoring multiple 160 m sections selected from a half factorial experimental design incorporating the following primary and secondary factors:

Primary	Secondary
Subgrade (fine/coarse)	AC drainage (yes/no)
Traffic (medium/heavy)	AC thickness
Temperature (freeze/non-freeze)	AC base type and thickness
Moisture (wet/dry)	Structural number of base and subgrade
	PCC drainage (yes/no)
	PCC strength and thickness
	Lane width
	Base type

 Accelerated pavement testing (APT) including road tests or accelerated loading facilities. Neither has been considered for implementation to date.

The GP and SP studies are further divided as follows:

•	GPS-1	Asphalt concrete (AC) on granular base
•	GPS-2	AC on bound base
•	GPS-3	Jointed plain Portland cement concrete (PCC) pavement
•	GPS-4	Jointed reinforced PCC pavement
•	GPS-5	Continuously reinforced PCC pavement
•	GPS-6A	Existing AC overlay on AC pavements
•	GPS-6B	New AC overlay on AC pavements
•	GPS-7A	Existing AC overlay on PCC pavements
•	GPS-7B	New AC overlay on PCC pavements
•	GPS-9	Unbounded PCC overlays on PCC pavements
•	SPS-1	Strategic study of structural factors for flexible pavements
•	SPS-2	Strategic study of structural factors for rigid pavements
•	SPS-3	Preventative maintenance effective for flexible pavements

SPS-4 Preventative maintenance effective for rigid pavements
 SPS-5 Rehabilitation of AC pavements
 SPS-6 Rehabilitation of jointed PCC pavements
 SPS-7 Bonded PCC overlays on concrete pavements
 SPS-8 Study of environmental effects in the absence of heavy loads
 SPS-9 Validation of SHRP AC specification and mix design (Superpave)

It appears that most of the sections have a thick asphalt or concrete surfacing contributing significantly to the structural capacity of the road.

The APT component has not been initiated to date, although the matter is being discussed at length in a number of fora¹¹. No formalised program of linking LTPP to APT at national level has been initiated, although this is being done to a limited extent in a number of states that have APT facilities.

2.2.2 Data Collection

A data collection guide⁹, supported by 22 detailed sub-documents, have been prepared as part of the LTPP project. The detailed guides include the following:

- Distress identification manual
- Falling Weight Deflectometer relative calibration analysis
- Guidance for rehabilitation
- Traffic data collection and processing
- FWD calibration protocol
- · Calibrating traffic data collection equipment
- Operational field guidelines for FWD measurements
- Operational field guidelines for profile measurements
- Test method for determining resilient modulus of unbound materials laboratory start-up and quality control procedure
- Test method for determining the creep compliance, resilient modulus and strength of asphalt materials using the indirect tensile test device
- Test method for determining the resilient modulus of unbound granular base/subbase materials and subgrade soils
- Seasonal monitoring program: Instrumentation installation and data collection guidelines
- Guide for field materials sampling, handling and testing
- Guide for laboratory material handling and testing
- Traffic monitoring guide
- SPS traffic site evaluation
- IMS reference material

- Climatic database revision and expansion
- · IMS quality control checks
- · Traffic quality control software

When compiling the documents, it was realised that the primary difficulties in utilisation of data collected in the past was the lack of uniformity of that data and the omission of data that was significant to the performance of the pavement. The data collection guides were therefore developed to support the experimental designs and provide a uniform basis for data collection. The approach taken identified those data items that were considered to be of high priority for achieving the goals of the LTPP studies. It also provided for a comprehensive set of other data items that may be desirable in the LTPP Information Management System for other purposes such as pavement management, detailed studies of pavement components, construction techniques and design features.

The following categories of data are collected:

- Inventory data
- Monitoring data
- Traffic data
- Climatic data
- Maintenance data
- Rehabilitation data
- Materials sampling and testing data

In addition to the above categories, a "minimum data set" considered to be the most desirable data set for fulfilling the requirements of the LTPP objectives was defined. This includes the dependent variables representing performance of pavements and those independent variables expected to significantly affect pavement performance.

Data collection and equipment used in each category is comprehensively described in the data collection manuals.

2.3. Australia and New Zealand

Sources of information:

- K Sharp and R Yeo, ARRB Transport Research
- R Douglas (University of Cantebury), D Alabaster and C Parkman (Transit NZ)
- Austroads reports

2.3.1 Background to ALF-LTPP

The objective of the Accelerated Load Facility - Long-Term Pavement Performance (ALF-LTPP) study is to compare the relative performance of full-scale in-service test sections under real traffic loading conditions with that determined under ALF loading. Verification of the relevance of accelerated pavement testing trials to observed in-service performance would result in an increased level of confidence in the use of these types of accelerated trials. Twelve sites are currently being monitored, although not all of the LTPP studies were initiated at the same time as the associated ALF program¹¹.

A comparative analysis conducted by Koniditsiotis (1999) suggested that there were clear benefits associated with conducting LTPP studies of pavement types already tested under accelerated loading conditions. In addition, the long-term monitoring of these sites would allow issues that cannot be addressed with accelerated loading, such as the effects of mixed traffic loading, environment and aging, to be evaluated.

2.3.2 Data Collection Protocols

Guidelines for site establishment and data collection have been prepared ¹². Since a number of the sites are official SHRP-LTPP sites, they are monitored according to the US standard described above.

New Zealand does not have a formal LTPP program. They have calibration sections for HDM models, but no links to their CAPTIF APT program. However, they are considering instrumenting one of the test sections in a similar manner to CAPTIF sections with a view to comparing performance predictions.

2.4. United Kingdom and Europe

Sources of information

- M Nunn and T Greening, TRL
- COST-347 Website

2.4.1 United Kingdom

The UK has a validation monitoring programme to assess the long-term performance of a number of designs on a number of pavements in the road network. However, since the UK APT programme is confined to a building where short specially constructed pavement sections are compared with control pavements, it is difficult to compare APT with LTPP, given the differences in construction technique. Where possible, TRL attempts to relate results from the APT programme to in-service performance, but this is done on a project-by-project basis and is dependent on funding.

2.4.2 **Europe**

There are some 17 APT facilities in Europe, mostly fixed in one location (ie cannot be moved between sites). No detail on comparison of the APT findings with that of LTPP findings has been located to date. However, the European Cooperation in the Field of Scientific and Technical Research (COST) programme is currently investigating the role of APT in pavement engineering. One of the tasks currently being carried out is a comparison between APT and LTPP research results. The study is concentrating on the following issues:

- Economics of APT vs LTPP
- Construction techniques
- Physical and environmental conditions
- Loading conditions
- Pavement deterioration

No results have been published to date. Another task will be to look at developing a common code of good practice. This entails two items:

- Guidelines for existing facilities
- Guidelines for new facilities

No reference to a protocol for comparing APT and LTPP sections could be located.

3. PROTOCOL DEVELOPMENT

Although numerous countries have an LTPP monitoring programme in place, it is clear from the literature review and interviews that only Australia has embarked on a dedicated comparison of APT results with those obtained from adjacent LTPP sections.

Since there is very little published information on the development of protocols to standardise the monitoring of LTPP sections in conjunction with APT sections, a workshop was held to brainstorm a framework for essential and desirable items that need to be monitored. The data that is currently being collected from HVS testing was used as a basis for this framework.

The framework will be developed into a detailed protocol for the establishment and operation of LTPP sections in conjunction with HVS tests. The requirements for calibration of performance models used in local pavement management systems will also be considered. The proposed chapters and subsections in the protocol include:

- Introduction
 - Background
 - Scope
- Linkage of HVS and LTPP
 - Justification of instrumentation
 - Justification of testing requirements
- Management and responsibilities
 - Staffing
 - Management structure and responsibility matrix
 - Funding
 - Data management
- Site location and establishment
 - Location and marking
 - Setting up
 - Instrument installation
- Data collection
 - Monitoring standards
 - Monitoring procedures
 - Sampling frequency
 - Laboratory testing
- Reporting criteria

Where appropriate, use will be made of relevant techniques developed for the SHRP program.

3.1. Problem Areas

In discussions on the development of a framework for the protocol, considerable debate arose around a number of issues. These included the minimum requirements for measurement and monitoring of deflection, transverse and longitudinal profile, moisture content and destructive vs non-destructive testing.

After considerable deliberation it was proposed that the following minimum standards should be included in the protocol, with the option of including additional measurements with other equipment resting with the road authority:

- Deflection On HVS sections, multi-depth deflectometers installed in the pavement at the same time as the HVS section. Periodic measurements with an RSD and FWD to determine maximum deflection and radius of curvature. On other LTPP sections, deflection measurements should be limited FWD.
- Transverse profile maximum depression under a 2.0 m straight edge using a 1.0 cm wedge.
- Longitudinal profile International Roughness Index (IRI) determined with any appropriate calibrated equipment meeting the specification for measuring HDM-III/IV sections. The equipment used must be specified in the database.
- Moisture twin probe nuclear density gauge with gravimetric calibration until a calibration curve is obtained for each LTPP section.
- Destructive testing will be confined to identified areas of the section such that they will not influence later monitoring.

It is also clear that there are ongoing developments in pavement monitoring techniques and equipment and laboratory testing. It is therefore suggested that the protocol is given a version number and that a statement to the effect that the document content will be reviewed periodically is included.

3.2. Linkage to Gautrans Database Project

The data outputs will be developed in the protocol and these will form the fields for the materials database currently being developed for Gautrans.

4. PROJECT PROGRAM

During preparation of this Inception Report, the overall project program and budget was reassessed. No significant changes in the program are envisaged and the budget will remain as quoted in the original proposal.

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APPENDIX B INSTRUMENTATION	

B.1 Road Surface Deflectometer (RSD)

B.1.1 Description

The RSD is a modification of the Benkelman Beam and measures the elastic surface deflection of a pavement under the action of a wheel load. The RSD consists of a 3.0 m long beam, which is supported on two reference feet at one end and the measuring point on the other. A Linear Variable Displacement Transducer (LVDT) is located between these two points. The RSD is positioned in such a way that the reference feet stand outside the deflection bowl area and the measuring point lies between the dual rear wheels of the measuring vehicle (two axle, dual tyre (11x20x14PR @ 520 kPa) truck with 8.2 tonne load on the rear axle). The deflection under the measuring point is then measured by logging the movement of the LVDT at various distances. At the measuring point a setscrew is located with which the RSD is zeroed before measurement starts.

B.1.2 Calibration

The RSD should be calibrated on the calibration jig, supplied with the instrument, prior to each set of measurements to ensure that the measured values are a true reflection of the actual deflection bowl. The calibration procedure is as follows:

- i) Select a smooth level surface.
- ii) Place the measuring point of the RSD on the jig plate
- iii) Set the RSD (software) and jig dial gauge to zero
- iv) Wind jig to 0.1 mm on the dial gauge and check the reading is the same on the RSD software
- v) Repeat the test at 0.1 mm intervals to 1.0 mm

B.1.3 Measurement Method

RSD measurements are taken as follows:

- i) Position the RSD on the painted marks (point at which the elastic surface deflection is to be measured) in the outer wheel path of Panel 1
- ii) Position the truck ±3.0 m from the end of the beam such that the beam lines up with the centre of the dual wheels
- iii) Start the test on the computer and reverse the test truck at creep speed \pm 1.0 m past the measuring point, towards the reference feet of the RSD
- iv) Move the wheel back to the starting point (± 3 metres away)
- v) Check that the reading has been taken
- vi) Repeat the test three times

vii) Repeat the test in each wheel track in each of Panels 1 to 10

B.1.4 Reporting

Peak deflection and deflection bowl are provided in electronic format.

B.2 Multi-Depth Deflectometer (MDD)

B.2.1 Description

The MDD consists of several modules with LVDTs, which are installed at various depths in the pavement. The MDD measures the elastic deflection and permanent deformation of the various layers in the pavement. The modules are installed at distances of not less than 150 mm apart inside a vertical hole in the pavement. Installation depths depend on the depths of the layers whose elastic deflection and permanent deformation are to be quantified and should be determined by the project engineer and project manager from DCP surveys, as-built data and/or test pits and cores as part of the HVS section design.

B.2.2 Installation

Installation of MDDs should be done as follows:

- Position marks for the MDDs should be painted on the outer wheel track 1.0 m from the end of Panel A and 1.0 m from the beginning of Panels B and C. A percussion drill and a specially designed drilling rig are used for drilling the holes, which are normally approximately 3.3 m deep and 36 mm in diameter. After each hole is drilled it is cleaned out with compressed air. A core drill should be used for the top 100 mm of the hole, especially if the pavement consists of asphaltic layers. Ream the top of the hole to a diameter of 90 mm and depth of 25 mm, or until the MDD top cap is level with the pavement surface after installation. Cut a 50 x 50 mm slot from the top of the hole to the road edge to accommodate the wiring.
- ii) Prepare the neoprene lining (0.08 mm thick neoprene rubber, formed round a stainless steel tube 33 mm diameter x 1 200 mm long) by covering the stainless steel tube with silicon grease placing then placing the rubber lining. Attach the aluminium bush with oil seal to the bottom end of the rubber lining.
- iii) Secure the anchor assembly in the hole with 200 m² of a mixture of cement and coarse river-sand in a ratio of 3 to 1.
- iv) Form the top cap with epoxy glue ensuring that it is positioned such that the screw holes in the top cap are in line with those in the cross section of the test section. The top cap must be left overnight for the epoxy to cure before the mould is removed.

- v) Mix the lining compound (2.0 t of Prostruct 34/40 and up to 300 mt xylene (depending on material) to liquidize the compound to a workable consistency, using a mixer connected to a hand drill) to secure the MDD anchor pin and the lining in the drilled hole. Pour the mixed liquid into the drilled hole, filling 50 per cent of the hole, to prevent air traps. Push the lining tube down into the hole while filling the hole with the remaining liquid. Use a neoprene cover around the hole to prevent spillage on the road surface. The lining compound will take between 12 and 48 hours to set, depending on the weather conditions (setting time increases with decreasing temperature). When set, remove the lining tube and cut the lining flush with the bottom of the top cap. Clean the lining with a cloth.
- vi) Fit the MDD snap connector onto the anchor pin using the supplied tool designed for this purpose.
- vii) Mark the MDD modules 1, 2, 3, etc. Ensure that each MDD slug has the same marks as its matching module. Do a final inspection on the modules to be used and check that all six securing ball bearings are fitted. Check that the cables are intact and properly soldered to each module.
- viii) Install the pilot rod (M5 brass rod, which is long enough to protrude ± 100 mm above surface) with the snap pin attached into the hole and ensure that the snap pin locks securely and positively in position. Write the depths at which the modules are located and the number of each module on the MDD information form. Clip the deepest installed module onto the MDD installation tool and mark on the tube of the MDD installation tool the desired depths of each module to be installed, using a marking pen. Measure from the centre of the securing ball bearings of the clipped on module to the prescribed depth. Guide the module to the deepest installed module position and with the MDD installation tool and pilot rod on the marked depth, secure the module with the MDD installation tool. Follow the same procedure with all the modules as required in this MDD hole. The sequence of modules is from the deepest, (with the highest number) to the shallowest, (No 1).
- ix) Feed the ribbon cables through the channels provided. The wires coming from levels 1, 2 and 3 modules on the module bodies are connected to the plug situated on the left-hand side of the top cap. The wires from levels 4, 5 and 6 are connected to the plug situated on the right-hand side of the top cap.
- x) Connect an installation unit to the MDD connections and check that every module is operating. This can be done with a dummy rod (M5 brass rod with length equal to the depth of the MDD hole and which has an MDD slug screwed onto its tip). While the rod is being pushed through the MDD modules fitted in the hole, the reading on the installation unit should be -13.00, 00.00, +13.00, as the slug on the dummy rod goes through each module.

- xi) Push another M5 rod with snap connector fitted into position in the hole until it clips into the snap connector. Mark the point at which the rod is flush with the surface of the test section with a marking pen or a strip of masking tape. Use the dummy rod to establish the position of the deepest MDD module by inserting it through the module until a zero reading is reached on the conditioner. Mark this depth with a marking pen or a strip of masking tape at the point on the road flush with the surface of the pavement. Repeat this operation with each module installed and mark each depth on the rod. Remove the marked rod from the MDD hole.
- xii) When assembling the MDD slug rod, attach a strip of masking tape on a flat working area. Place the rods on the working place alongside the masking tape. Mark the total depth from the dummy rod onto the tape. Mark the locations of the MDD slugs for each module as marked on the rod.
- xiii) With the markings on the strip of masking tape, assemble the MDD slug rod starting from the snap connector pin. Place the numbered slug of each MDD on its mark on the masking tape. Place the snap connector pin on the snap connector pin mark from the reference point and cut lengths of M3 brass threaded rod to connect the snap connector pin and each slug forming the MDD slug rod. Use M3 brass threaded taper ferrules to lock the lengths of rods into the slugs.
- xiv) Screw a ±300 mm long rod onto the top slug. Do not lock with a ferrule, as the rod is used for handling the MDD slug rod and will be removed after completion of installation. Push the MDD slug rod into the MDD hole through the modules until it snaps on the snap connector on the anchor pin.
- xv) The final adjustments to the slug positions can be made, based on the readings on the different channels on the installation unit, in order to have the slug located in the correct position. Shortening of the rod results in positive readings and lengthening of the rod in negative readings.
- xvi) Once the correct readings are obtained, thread the wires into a conduit and embed it in the prepared slot with cold mix patching material. Bury the conduit in the road reserve and connect to a plastic box that will house the connector. Ensure that the box is sealed and secured.

Detailed tool and equipment lists are provided in the HVS Operations Protocol.

B.2.3 Calibration

After the installation of the MDD modules at the desired depths, the MDD must be calibrated. This will ensure that the measurements agree with the actual movement in the pavement. The HVS technician is responsible for the calibration of the MDD.

The following tools are required to calibrate the MDD modules fitted into an MDD hole:

- A calibration unit (part of the data acquisition software)
- A calibration jig fitted with a dial indicator mounted into a screw adjusting mechanism

The calibration process is as follows:

- i) Remove the snap connector pin from the MDD slug rod in order to facilitate free movement of the slug assembly. Move the MDD slug rod up and down to determine the mid (zero) position of the module (ie -13.00, 00.00, +13.00).
- ii) Place the calibrator unit above the MDD hole and connect the MDD slug rod with the calibrator unit. Turn the screw mechanism until the deepest module reads 0.00 on the conditioner unit.
- iii) Set the dial gauge on the screw mechanism to a zero reading and turn the screw mechanism until the reading is 7.5 mm on the dial gauge (using an E300 LVDT).
- iv) The same procedure is repeated for the calibration of the other modules. When the calibration procedures are complete replace the snap connector pin on the MDD slug rod and enter the final pot setting readings on the MDD information form.
- v) Do a final general inspection of the installation and connections and close the top cap.

B.2.4 Measurement Method

MDD measurements are downloaded into a data acquisition system.

B.2.5 Reporting

Permanent deformation and elastic deflection are provided in electronic format.

B.3 Temperature Buttons

B.3.1 Description

The temperature button is a computer chip enclosed in a 16 mm stainless steel casing that stores temperature data in a range between -10 and 85°C. It is designed to withstand harsh conditions.

B.3.2 Installation

Temperature buttons are installed as follows:

 Drill a ? diameter hole to the required depth (typically bottom of the surfacing) in the required position (centre of the lane in Panels A, B and C)

- Place thin levelling layer of sand on the bottom of the hole
- Set temperature button to the required recording interval (120 minutes)
- Place temperature button in the bottom of the hole
- Seal the hole with cold mix filler, ensuring that there is no protruding aggregate

B.3.3 Calibration

Temperature buttons can be calibrated in hot water, by checking the temperature of the water and then immersing the button and checking the temperature recorded.

B.3.4 Measurement Method

Temperature buttons must be extracted from the pavement to download the data. This should be done carefully to prevent damage. Once removed, the data should be downloaded. The button can then be cleaned, calibrated and replaced in the hole.

B.3.5 Reporting

Data is captured electronically and presented in spreadsheet compatible format.

B.4 Dual Probe Hydro-density Meter

B.4.1 Description

The dual probe hydro-density meter (Strata gauge) is used to measure density and in-situ moisture content of the pavement structure. Measurements are recorded in 50 mm increments to a depth of 600 mm. The source material in the hydro-density meter is radioactive and although this does not pose a hazard to the operator under normal operating conditions, strict operating, maintenance and transport procedures, supplied with the equipment, must be followed at ala times. Certain legal requirements in this regard must also be followed.

B.4.2 Calibration

The hydro-density meter should be calibrated on standard blocks according to the manual supplied with the instrument. Calibration blocks are available at the CSIR.

B.4.3 Measurement Method

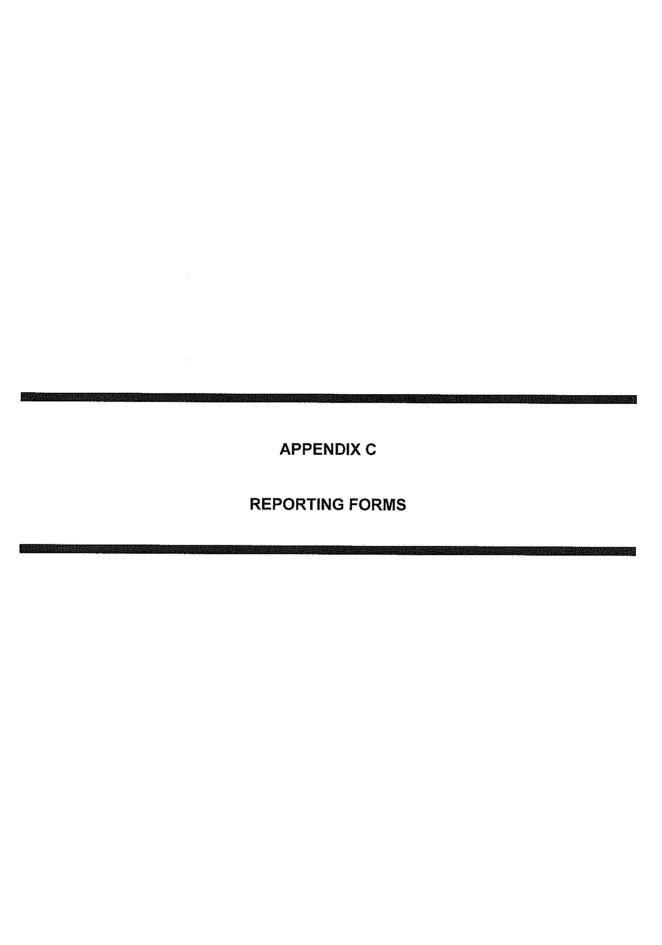
The following procedure should be followed:

- i) Remove the cap of the predrilled holes.
- ii) Drop a 1.0 m x 10 mm wooden dowel into the hole to check for standing water/mud. If the holes have standing water/mud, new holes will have to be drilled 30 cm along the wheel track from the previous hole.

- iii) Measure the density and moisture at 50 mm intervals, starting at 600 mm, strictly following the specific operating and safety instructions provided with the gauge.
- iv) Record the information on the LTPP Density and Moisture Form (Appendix C).
- v) Reseal the holes.

B.4.4 Reporting

Density and moisture content are recorded on an LTPP density and moisture content form.



APPENDIX C: REPORTING FORMS

The following forms for the monitoring of LTPP sections are provided:

- Visual assessment (Form 1)
- Profile (Form 2)
- Density and moisture content (Form 3)
- Dynamic cone penetrometer (Form 4)
- Weather (Form 5)
- Test pits (Form 6)
- RSD Calibration (Form 7)
- MDD Calibration (Form 8)

Data for deflection, permanent deformation and traffic will be provided electronically in a spreadsheet or spreadsheet compatible format.

		LIP	****		L A	SSE	SSN	IENT		₹M				Fo	rm 1
LTPP Section			Pa	anel				Da				Eva	luator		
						St	ırfac	ing a	sses	smei	nt				
Surfacing type													***************************************		
Texture	Va	rying]	Fine		F - N	1	Med	ium	М	- C	Course			
Voids	Va	rying		Vone		N - I	-	Fe	W	F	- M	Many	1		
			De	gree					Exter	nt		Length	Width	Number	Panels
	Slig	ght			Se	vere	Slig	ght		Se	vere	Longui	, vidii	Namber	I aneis
Mechanical failure	0	1	2	3	4	5	1	2	3	4	5				
Other failure	0	1	2	3	4	5	1	2	3	4	5				
Bleeding/flushing	0	1	2	3	4	5	1	2	3	4	5	Narrow	Wide	Position	_
Surface cracks	0	1	2	3	4	5	1	2	3	4	5				*****
Binder condition	0	1	2	3	4	5	1	2	3	4	5	Active	Stable	Position	ļ
Aggregate loss	0	1	2	3	4	5	1	2	3	4	5		7	1	
						Sti	uctu	ral as	ses	smer	nt	1	-I. , , ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		.l.,
			De	gree				Ī	Exter	ıt	•	Narrow	Wide	D10	B
	Slig	iht			Se	vėre	Slig	jht		Se	vere	(% area)	(% area)	Position	Panels
Cracks - block	0	1	2	3	4	5	1	2	3	4	5				
Cracks - longitudinal	0	1	2	3	4	5	1	2	3	4	5			***	
Cracks transverse	0	1	2	3	4	5	1	2	3	4	5				*******
Cracks - crocodile	0	1	2	3	4	5	1	2	3	4	5	· · · · · · · · · · · · · · · · · · ·			
Cracks - parabolic	0	1	2	3	4	5	1	2	3	4	5				
Pumping	0	1	2	3	4	5	1	2	3	4	5		1		
Rutting	0	1	2	3	4	5	1	2	3	4	5	1			
Undulation/settlement	0	1	2	3	4	5	1	2	3	4	5	-			
Edgebreak	0	1	2	3	4	5	1	2	3	4	5	Number	Diameter		
Potholes	0	1	2	3	4	5	1	2	3	4	5		Γ		
Delamination	0	1	2	3	4	5	1	2	3	4	5				
	. ,	<u> </u>				L			L			Small	Medium	Large	Panels
Patching	0	1	2	3	4	5	1	2	3	4	5				
		L			L	Fur	ctio	l nal as		smer	nt	<u> </u>			
			Deg	ree	 	<u> </u>	19 4 5 1 1 1 1 1 1	er en en en	xten	Arriva.		<u> </u>			<u> </u>
	Slig	ht			Sev	/ere	Slig	4.2	· · .		vere		influenc	ing factors	
		1	2	3	4	5	1	2	3	4	5	Potholes	Patching	Undulation	Corrugat
Riding quality	0				4	5	1	2	3	4	5	Bleeding	Polishing		
Riding quality Skid resistance	0	1	2	3					3	4	5		3	<u> </u>	
Skid resistance		1	2	3	4	5	1	2	J						
	0				4	5 5	1	2	3	4	5			•	

			,	L	TPP	PRO	FILI	E AS	SES	SME	NT F	ORN	ſ							Forr	n 2	
L	TPP Sectio	n			· ··············	Pa	nel	1	- 5	1	Date				E	valua	tor					
	Panel A		1.9	1.8	1.7	1.6	1.5	1.4	1,3	1.2	1.1	1.0	6.0	0.8	0.7	9.0	0.5	0.4	0.3	0.2	0.1	RE
	Max rut	Lane Centre																		-		
	Width	Lane		ļ							ļ											
			2.1	2.2	2.3	2,4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	궁
	Panel 1 Max Rut	ıntre	1.9	1.8	1.7	1.6	1.5	1.4	1.3	1.2	1.1	1.0	0.9	0.8	0.7	9.0	0.5	0.4	0.3	0.2	0.1	뿐
	Width	Lane Centre																				
			2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	占
	Panel 2		1.9	8 -	1.7	1.6	1.5	4	6.	1.2	1	0.1	6.0	0.8	0.7	9.0	0.5	4.0	0.3	0.2	1.0	뿐
	Max Rut	Lane Centre																				
	Width	Lane																				
verse			2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	ರ
Transverse	Panel 3		6:	1.8	1.7	9.1	5.	4 -	<u></u>	1.2	-	1.0	6.0	0.8	0.7	9.0	0.5	4.0	0.3	0.2	0.1	믮
	Max Rut	Lane Centre													į.							
	Width	Lane																				
	D14		2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	ፘ
	Panel 4			1.8	1.7	1.6	1.5	4 1	1.3	1.2	-	0.	0.9	0.8	0.7	9.0	0.5	0.4	0.3	0.2	0.1	쀭
-	Max Rut	Lane Centre																				
	Width	Lane												:								
			2.1	2.2	2.3	2,4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3,4	3.5	3.6	3.7	3.8	3,9	ರ
	Panel 5		6.	1.8	17	1.6	1.5	1.4	£ _	1.2	11	1.0	6.0	9.0	0.7	9.0	0.5	0.4	0.3	0.2	0.1	RE
	Max Rut	Lane Centre							:													
	Width	Lane (~~~											
			2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	ರ
밀	Position Outer		1	 	2	2		3	4			5 	6)	7	,	8	}	5)	1	0
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Long	Lane centr	e																				·
	Lune Ochiu											ļ										

				L	TPP	PRC	FILE	E AS	SES	SME	NT F	ORN	ń.							Forn	n 2	
LT	PP Section	n				Par	nel	6	- 10		Date				Εν	/alua	tor					
	Panel B		6.1	1.8	1.7	1.6	1.5	1.4	1.3	1.2	-	1.0	0.9	0.8	0.7	9.0	0.5	0.4	0.3	0.2	0.1	RE
	Max Rut	Lane Centre																				
	Width	Lane		ļ					ļ													
			2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	က 8	3.9	占
	Panel 6 Max Rut	Te	1.9	1.8	1.7	1,6	1.5	1.4	1.3	1.2	1.	1.0	6.0	0.8	0.7	9.0	0.5	0.4	0.3	0.2	0.1	RE
	100 10	Lane Centre										· · · · · · · · · · · · · · · · · · ·										_
	Width	נ	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	ا ا
	Panel 7		6.	1.8	1.7	1.6	1.5	4	1.3	1.2	1-	10	6.0	0.8	0.7	9.0	0.5	4.0	0.3	0.2	0.1	H.
	Max Rut	Lane Centre																				
ė	Width	Lane	· . · · · ·																			
Transverse	D10		2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	占
Tran	Panel 8 Max Rut	e	1.9	1 .8	1.7	1.6	7.5	4.1	1.3	1.2	1.1	- 0	6.0	0.8	0.7	0.6	0.5	0.4	0.3	0.5	0.7	RE .
	· · · · · · · · · · · · · · · · · · ·	Lane Centre															········					
	Width	Le	2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	占
•	Panel 9		1.9	1.8	1.7	1.6	1.5	1.4	6.	1.2		1.0	0.9	0.8	0.7	9.0	0.5	0.4	0.3	0.2	0.1	Ж Ж
	Max Rut	Lane Centre	·							-	· .								*. *			
-	Width	Lane					:															
			2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	딩
	Panel 10			Ф,	1.7	1.6	1.5	1.4	1.3	1.2	1.1	1.0	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.2	0.1	뀖
	Max Rut	Lane Centre								-												
	Width	Lane	_			-	. IO			3				<u></u>								
\perp			2.1	2.2	2.3	2.4	2.5	2.6	2.7	2.8	2.9	3.0	3.1	3.2	3.3	3.4	3.5	3.6	3.7	3.8	3.9	김
Notes																	1				:	

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LTPP S				Date			Evalua	tor			•	
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Std wet		14	A -4I		L	<u> </u>	 .	1	<u>.L</u>	ļ	<u> </u>	
	Probe	Input	Actual		er wheel			er wheel		107.4	Centrelin	
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Panel A	14	200	350	1		 		-	 	1	 	
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	16	200	400			 						<u> </u>
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Panel B	12	200	300						 			<u> </u> -
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- 1	Sample	e T	in No	1	MC	Actual		MC	Actual	T	MC	Actual
	depth	_ _				dry			dry		1110	dry
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Panel A		-		-						1		
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8 C [7111711			
Panel C												
[*****	,				*******	

		LTP	P DCP RECO	ORDING SHE	ET			Form 4
LTPP	Section		Panel	D	ate	Ope	rator	
	Outer whee	l track		nner wheel	track		Centre	line
0			0			0		
5	205	405	5	205	405	5	205	405
10	210	410	10	210	410	10	210	410
15	215	415	15	215	415	15	215	415
20	220	420	20	220	420	20	220	420
25	225	425	25	225	425	25	225	425
30	230	430	30	230	430	30	230	430
35	235	435	35	235	435	35	235	435
40	240	440	40	240	440	40	240	440
45	245	445	45	245	445	45	245	445
50	250	450	50	250	450	50	250	450
55	255	455	55	255	455	55	255	455
60	260	460	60	260	460	60	260	460
65	265	465	65	265	465	65	265	465
70	270	470	70	270	470	70	270	470
/5	2/5	475	75	275	475	75	275	475
80	280	480	80	280	480	80	280	480
85	285	485	85	285	485	85	285	485
90	290	490	90	290	490	90	290	490
95	295	495	95	295	495	95	295	495
100	300	500	100	300	500	100	300	500
105	305	505	105	305	505	105	305	505
110	310	510	110	310	510	110	310	510
115	315	515	115	315	515	115	315	515
120	320	520	120	320	520	120	320	520
125	325	525	125	325	525	125	325	525
130	330	530	130	330	530	130	330	530
135	335	535	135	335	535	135	335	535
140	340	540	140	340	540	140	340	540
145	345	545	145	345	545	145	345	545
150	350	550	150	350	550	150	350	550
155	355	555	155	355	555	155	355	555
160	360	560	160	360	560	160	360	560
165	365	565	165	365	565	165	365	565
170	370	570	170	370	570	170	370	570
175	3/5	5/5	1/5	375	575	175	375	575
180	380	580	180	380	580	180	380	580
185	385	585	185	385	585	185	385	585
190	390	590	190	390	590	190	390	590
195	395	595	195	395	595	195	395	595
200	400	600	200	400	600	200	400	600
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Rain Max Min Rain	Min	c	1				May			June	
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Surface fluyer bond Structure Soil type Origin Sample					LTPP TEST PIT FORM	PIT FORM	Variable Control of the Control of t				Form 6	
Moisture Colour Consistency Structure Soil type Origin Disturbed Undisturbed Sample	LTPP Section	on:		Panel:		Position			Pre	ofiled by:	*104140	
Moisture Colour Consistency Structure Soil type Origin Sample	Surface/la	yer bond		. *************************************				A CANAGE OF		The state of the s	774111	
Sample S	Depth	Moisture	Colour	Consistency	Structure	Soil type	Origin	Disturbed	Undisturbed		Comments	
Cracks	(mm)					-		sample	Sample			
Cracks Cracks Description Carbonation		TOTAL SECTION AND A SECTION ASSESSMENT AND A SECTION ASSESSMENT AS								1111		
Cracks C	to											
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Rutting Heaving Interface bond Moisture at interface Carbonation		Cracks		Description		0.04440			- Thirting			
	Checklist	Rutting		Heaving				Moisture at inte	rface	Layer definiti		
	·· <u>··</u> ···	Carbonation										

LTPP I	RSD CALIBRATION S	SHEET	Form 7
LTPP Section No:		Panel:	
Date:		Calibrated by:	
Duto.	 	Calibrated by.	
RSD ID No:		I I avail Nia	
RSD ID NO.		Level No:	
Dial gauge	Computer Up	Computer Down	Difference
0.0			
0.1			
0.2	10-7/1		
0.3			
0.4			
0.5			
0.6	*****		
0.7			
0.8			
0.9			
1.0			
		Average	
	The	refore mm/v = 1/average	
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Signati	ıre		
Olgilati		-	
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LTPP MULTI DEPTH	I DEFLECTOMETER C		Form 8
LTPP Section No:	TOWNS -	Panel:	
Date:		Calibrated by:	
MDD No:		Level No:	
Dial gauge	Computer Up	Computer Down	Difference
0			
1			
2			
3	,		
4			
5	···········		
6			
7	**********		
8			
9	********		****
10			
, —		Average	
	The	refore mm/v = 1/average	
MDD No:		Level No:	
Dial gauge	Computer Up	Computer Down	Difference
0			
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2 3	***************************************		

4			
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6 7	Ç		
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10	10410000000	A)	V/IIIVI-
	The	Average	
	ITIE	refore mm/v = 1/average	, , , , , , , , , , , , , , , , , , ,
MDD No:		Level No:	
Dial gauge	Computer Up		Difference
Diai gauge 0	- Computer op	Computer Down	Difference
1	, market		
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3			······································
4			. S. M. W. C
5			
6	, , , , , , , , , , , , , , , , , , ,		
7			· · · · · · · · · · · · · · · · · · ·
8			
9	. , ,	1	
10			
		Average	***************************************
	Ther	efore mm/v = 1/average	
			The state of the s
Signa	ture		3